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Research Article

Tidal Current Energy Resources Assessment in the Patinti Strait, Indonesia

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ABSTRACT. Indonesia is currently intensively developing its renewable energy resource and targets at least 23% by 2025. As an archipelago country, Indonesia has the potential to benefit from its abundant renewable energy resources from its offshore regions. However, the short tidal range of mixed semi-diurnal and the suitable tidal turbine capacity may hinder marine renewable energy development in Indonesian waters. This paper presents higher-order hydrodynamic numerical models to provide spatial information for tidal current resource assessment of the Patinti Strait. The present study applied the hydrographic and oceanographic method to produce input of the numerical model. Based on the selected simulation analysis, the highest current speed could be identified around Sabatang and Saleh Kecil Island with up to 2.5 m/s in P1 and 1.7 m/s in P4. Besides, the operational hours for the two observation points are 69% and 74.5%, respectively. The results indicate that this location is of prime interest for tidal turbine implementation as an energy source, for medium capacity (300 kW) and high capacity (1 MW).

Keywords: Tidal current, renewable energy, resource assessment, numerical model, Indonesia

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1. Introduction

Global warming has been alarming in the past years, as the earth temperature increases by 0.08°C per decade (NOAA, 2020). This evidence is backed by a study demonstrating that atmospheric CO₂ reached over 400 ppm in 2018 and went over the natural state, which was between 170 to 300 ppm (Ritchie & Roser, 2017). A number of local, regional or even global efforts are initiated, aiming to slow down the temperature rise, and the most addressed issue is arguably the plan for reducing dependency on fossil fuel. Currently, oil, gas and coal account for more than 80% of primary energy consumption (BP, 2019). The utilisation of low-carbon energy is expected to meet the energy demand while substituting these conventional energy sources.

At present, Indonesia relies heavily on conventional energy resources such as oil, gas and coal. In densely populated islands, such as Java and Sumatra, the operational cost for oil, gas, or coal energy is at an economically feasible level (Ministry of Energy and Mineral Resources of the Republic of Indonesia, 2018).

However, this does not apply to small, remote and less populated islands where the operational cost can be significantly higher because of expensive logistics. Moreover, these unsustainable energy resources are limited and will have to be supplemented by a renewable source of energy in the future.

The 23% renewable energy target in 2025 has become an urgent issue for Indonesia (PLN, 2017). Marine energy is listed as one of the renewables, which the technology classified into the tidal barrage, tidal current, waves, ocean thermal energy, and salinity gradients (OES, 2019). Tidal barrage offers a mature technology such as the one demonstrated in La Rance, France. However, it requires a massive coastal dam to create a head differential. Furthermore, Indonesia's tidal range is not too high to produce a consistent current speed required to drive the turbine. Among the other technologies, tidal current is more preferred because of its predictability and technology advancement. This paper then discusses the condition of tidal current in the Patinti Strait concerning the type of turbine to be used.

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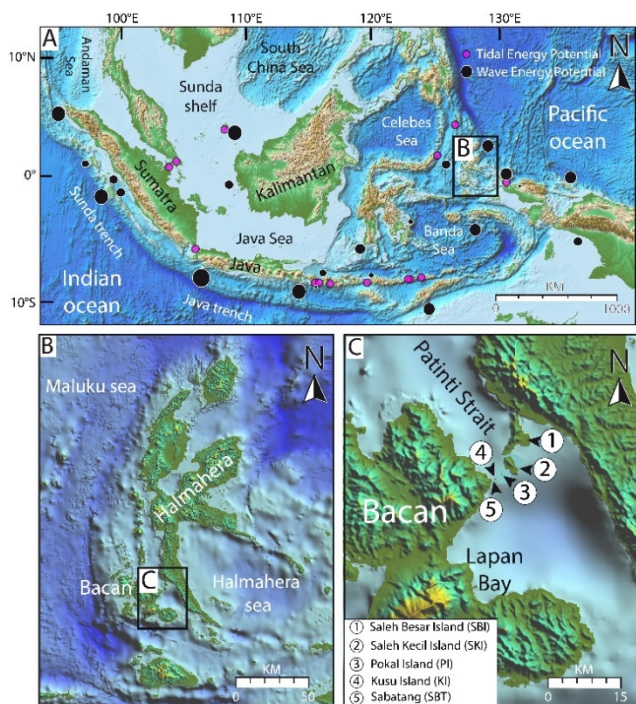


Fig. 1 (A) The regional and (B–C) local study area. (Source: <https://earthexplorer.usgs.gov/>)

As an archipelago country, Indonesia is suitable for the exploitation of a marine renewable energy source, as the potential tidal current and ocean wave energy is enormous (Fig. 1A). Currently, three straits have been studied extensively for tidal current energy development, namely Lombok, Alas and Larantuka Straits, located in Bali, Nusa Tenggara region (Blunden *et al.*, 2013; Orhan *et al.*, 2015; Firdaus *et al.*, 2019; Firdaus *et al.*, 2020; Orhan & Mayerle, 2020). Besides, researchers have also demonstrated potential in other sites such as Kelabat Bay, Sunda, Boleng, Molo, and Pantar Straits (De Groot, 2012; Sudjono *et al.*, 2014; Novico *et al.*, 2015; Ajiwibowo *et al.*, 2017; Pratama *et al.*, 2020). Furthermore, summaries on multiple tidal current energy sites are provided in several previous studies (Susilohadi *et al.*, 2014; Kementerian ESDM, 2017). Even though Indonesia has enormous ocean and many narrow straits, the number of prior studies related to the possible implementation of marine renewable energy in Indonesia is still limited.

North Maluku Province is one of the national targets for research related to marine renewable energy. It is one of the national fish barns that still have a deficit of energy in their remote area. Furthermore, Rahmawati (2017) revealed that several offshores in North Maluku have potency for tidal current energy. Thus, the study on tidal currents has been completed in this province, particularly in Patinti Strait. The Patinti Strait is one of selected locations for research by the Indonesia Ministry of Energy and Mineral Resources. This activity is part of updating the ocean current energy potential maps of Indonesia.

The Patinti Strait (PS) is located between Bacan Island (BI) and Halmahera Island (Fig. 1B). The smallest width of the PS is approximately 16.33 km, with several islands in this region. The Saleh Besar Island (SBI) is the largest island; the others are Saleh Kecil Island (SKI), Kusu Island (KI) and Pokal Island (PI) (Fig. 1C). The strait depths vary, ranging from depths of 10 m to 500 m in the northern part of SBI and 20 m to more than 1500 m in the

southern part (Pushidros TNI AL, 2011). The depth near KI and PI is less than 200 m. Local inhabitants stated that the life risk for people under taking maritime activities like vessel traffic in this area is very high because of its unpredicted high currents and waves. They called this region Tanjung Neraka, translated as 'Sabatang' (SBT), one of the most dangerous zones within the PS, which is typically avoided by ships and fishermen during the occurrence of high currents and waves. By contrast, this strait is one of fishermen's favourite sites because it has abundant fish resources. Despite this economic potential, this area is still slow because of a lack of energy supply in this underdeveloped region. For example, cold storage could not be maximised to support local fishery activities because of the lack of electricity supply.

2. Materials and Methods

2.1 Data Acquisition

The field survey in the PS was carried out to obtain the data to develop a numerical model and an energy resource assessment analysis. It included a high-precision single-beam echo-sounder survey, with tidal observation at three locations, namely Gilalang, Tomara and SKI, and two static Acoustic Doppler Current Profiler (ADCP) measurements were performed for 1 month on April 2017 in two locations at the study area, Fig. 2. The current observations were located in the narrow part of the PS. ADCP measurements provide important characteristics of tidal currents such as speed, direction, vertical stratification and through-flow (Susanto *et al.*, 2013). This measurement method has been implemented for long-term measurement at several places, for example, in the Black Sea (Zatsepin *et al.*, 2012; Piotukh *et al.*, 2016).

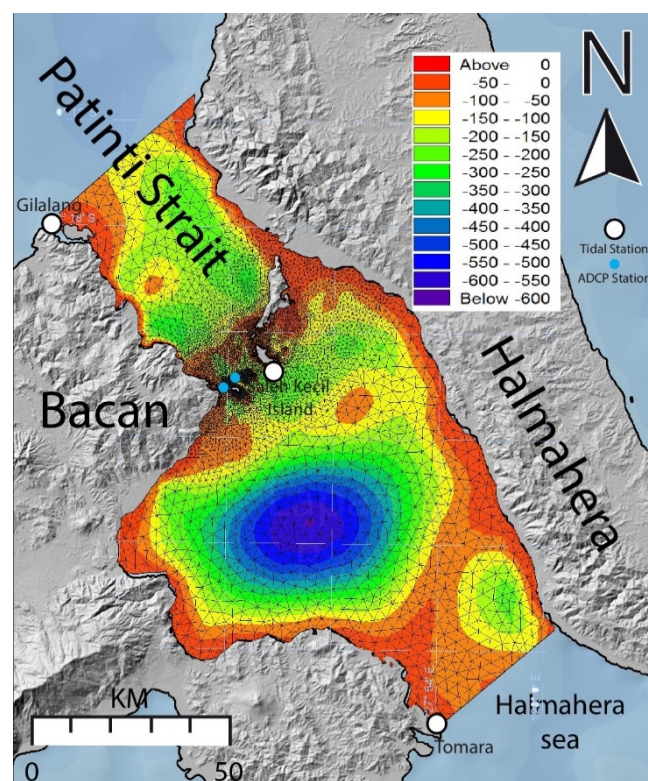


Fig. 2 Model mesh of the study area with bathymetry (depth is in Chart Datum; map projection is UTM 52S)

The bathymetry data from the survey campaign are utilised as a primary input for the model mesh, whereas the water level and current measurements are for model calibration and validation purposes.

2.2 Two-dimensional Hydrodynamic Model

Hydrodynamic conditions are essential for the study of marine renewable energy (Woolf *et al.* 2014). The utilisation of hydrodynamic numerical modelling is mainly for the assessment of an energy resource and its environmental impact. The hydrodynamic model provides spatial information on a time period as an input for the resource assessment analysis in more efficient time and cost compared to other methods, such as direct measurement. This approach has been successfully implemented in several locations, such as Rathlin Sound, Northern Ireland (Ortiz *et al.*, 2017), the northern part of Scotland and the Irish sea (Neill *et al.*, 2017), the Gulf of Mexico and the east coast of Florida, United States (Dhanak *et al.*, 2016), the Bay of Fundy and the Gulf of Maine, Canada (Hasegawa *et al.*, 2011), Zhoushan (Yu *et al.*, 2017), the Eastern Region of Pingtan Island (He *et al.*, 2017), and the Qiongzhou Strait (Wu *et al.*, 2016) in China. The hydrodynamic conditions for the energy resource assessment in this study are based on the local scale numerical model simulation using MIKE 21 software package (flow model FM module). The model is a two-dimensional state of the art with a flexible mesh based on the Navier–Stokes equation (DHI, 2012). The flexible mesh is able to resemble a complex coastal geometry and offers smooth domain downscaling, from a coarse mesh at the boundary to a finer resolution at the area of interest.

The software is governed by the integrated horizontal momentum equation and the continuity equation. The two-dimensional shallow water equation is shown by Eq (1)-(3):

$$\frac{\partial h}{\partial t} + \frac{\partial h\bar{u}}{\partial x} + \frac{\partial h\bar{v}}{\partial y} = hS \quad (1)$$

where each of the horizontal components of the formula are shown as:

$$\begin{aligned} \frac{\partial h\bar{u}}{\partial t} + \frac{\partial h\bar{u}^2}{\partial x} + \frac{\partial h\bar{u}\bar{v}}{\partial y} &= f\bar{v}h - gh\frac{\partial\eta}{\partial x} - \frac{h}{\rho_0}\frac{\partial p_a}{\partial x} - \frac{gh^2}{2\rho_0}\frac{\partial\rho}{\partial x} + \frac{\tau_{sx}}{\rho_0} - \frac{\tau_{bx}}{\rho_0} - \\ &\frac{1}{\rho_0}\left(\frac{\partial s_{xx}}{\partial x} + \frac{\partial s_{xy}}{\partial y}\right) + \frac{\partial}{\partial x}(hT_{xx}) + \frac{\partial}{\partial y}(hT_{xy}) + hu_s S \end{aligned} \quad (2)$$

and

$$\begin{aligned} \frac{\partial h\bar{v}}{\partial t} + \frac{\partial h\bar{v}^2}{\partial y} + \frac{\partial h\bar{u}\bar{v}}{\partial x} &= -f\bar{u}h - gh\frac{\partial\eta}{\partial y} - \frac{h}{\rho_0}\frac{\partial p_a}{\partial y} - \frac{gh^2}{2\rho_0}\frac{\partial\rho}{\partial y} + \frac{\tau_{sy}}{\rho_0} - \frac{\tau_{by}}{\rho_0} - \\ &-\frac{1}{\rho_0}\left(\frac{\partial s_{yx}}{\partial x} + \frac{\partial s_{yy}}{\partial y}\right) + \frac{\partial}{\partial x}(hT_{xy}) + \frac{\partial}{\partial y}(hT_{yy}) + hv_s S \end{aligned} \quad (3)$$

The depth-averaged velocities are defined by Eq (4)

$$h\bar{u} = \int_{-d}^n u dz \quad \& \quad h\bar{v} = \int_{-d}^n v dz \quad (4)$$

The numerical model domain extends along the entire PS between BI and Halmahera Island (Fig. 2). In most of the model domain, the bathymetry input for the model is retrieved from the GEBCO 2014 database with a resolution of 30 arc-seconds (Weatherall *et al.*, 2015).

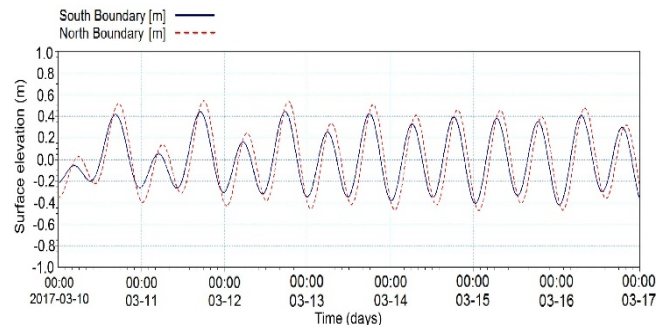


Fig. 3 The tidal elevation boundary condition at the north and south boundary

Around the proposed turbine location, close to SKI, the bathymetric data are supplemented by the detailed data from the field survey campaign described in the previous section. Both bathymetry datasets are combined and georeferenced to the benchmark spot (chart datum). The grid resolution ranges from 1 km for the outer part of the model domain to 50 m on the narrow part of the strait where the proposed turbine is located.

The tidal information at boundaries is calculated from DHI's Global Tide Model (GTM). The GTM is based on TOPEX/POSEIDON altimetry data with a resolution of 0.125° constructed from major diurnal (K1, O1, P1 and Q1) and semi-diurnal constituents (M2, S2, N2 and K2). Figure 3 illustrates the tidal variation at boundary conditions that indicate the tidal amplitude and phase differences between the two boundaries as the driving force of the hydrodynamic process. To ensure that the boundary information is accurate, the water level data derived from the TOPEX altimetry dataset have also been quantitatively validated to the ADCP measurements in the Japan Sea and it is confirmed as reliable (Ebuchi & Hanawa 1995). In this study, the tidal level for the boundaries of the strait has been validated with the field measurements from the survey campaign.

2.3 Resource Estimation Theory

The fundamental criteria to determine tidal energy deployments' successful implementation are power density, scalability, durability, maintainability, economic feasibility and environmental impact (Roberts *et al.*, 2016). To align with the principle of tidal energy deployments, a multi-criteria assessment methodology is critical in estimating the power potential harvested from the turbine.

Several reference studies have reviewed the best approach to optimising energy to be harvested. Examples are the fundamental formula behind the tidal turbine by Bryden *et al.*, (2007), characteristics of the velocity profile and the seabed friction for reduction of the tidal velocity by Lewis *et al.*, (2017), power generation as a function of horizontal axis of the turbine using the modelling approach by Mungar (2014) and tidal farm arrays for optimising the resource assessment by Lewis *et al.*, (2015).

A resource energy assessment is also carried out to determine a suitable location for the turbine, selected through a multi-criteria analysis that accounts for the physical and environmental constraint. The criteria for the resource assessment are as follows:

- Hydrodynamic conditions: The assessment is based on the current speed condition from the hydrodynamic model simulation. Furthermore,

average kinetic power densities are calculated using the following formula (Bryden *et al.*, 2007):

$$P = \frac{1}{2} \cdot \rho \cdot U^3 \quad (5)$$

P is tidal stream power per unit area of flow, ρ is the density of seawater, and U is the current speed. The value used as the current speed is the undisturbed speed, where a tidal turbine is not involved in speed reduction due to energy extraction.

- Depth: The assessment follows two conditions; high capacity from 40 to 100 m and low capacity from 10 to 40 m.
- Cut-in speed: the assessment is performed for cut-in speeds of 0.2 m/s and 0.4 m/s.

3. Result and Discussion

3.1 Model Validation

The numerical model is validated with the survey measurements at two stations in the study area, the surface elevation data at SKI station (longitude: 127.7356°, latitude: -0.4295°) and current at SBT Station (longitude: 127.7036°, latitude: -0.4498°).

Based on the tidal and current residual analysis, the sites' hydrodynamic condition is predominantly tidal force, and the non-tidal components such as wind and surge are not significant. Therefore, model validation over the measurement period on March 2017 is valid for representing the annual condition.

Validation performance of the model for tide-driven current is illustrated in Fig. 4 and Fig. 5. The tidal current component from the measurement data is used for comparison at the validation process (Isobe *et al.*, 2007). The comparison between the model and the measurements data (Figs. 4 and 5) indicates that the water level and current from the simulation are a reasonably close match and indicates a satisfactory agreement between the model and the measurements.

A validation requirement for hydrodynamic conditions for coastal application (Evans, 1993) is the root mean square error (RMSE) of the water level within 10% of spring tidal range or 15% of the neap tidal range 10%–20% of the measured current speed. The RMSE formula is as follows:

$$RMSE = \sqrt{\frac{\sum_{i=1}^n (\text{Predicted}_i - \text{Actual}_i)^2}{n}} \quad (6)$$

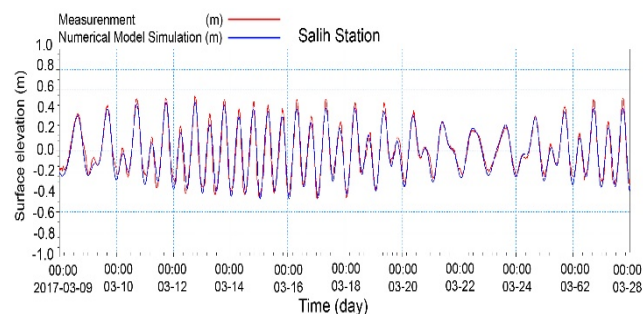


Fig. 4 Water level comparison between model simulation results and measurement at the SKI station (RMS error: 6.56 cm within an acceptable criteria range of 9.58 cm).

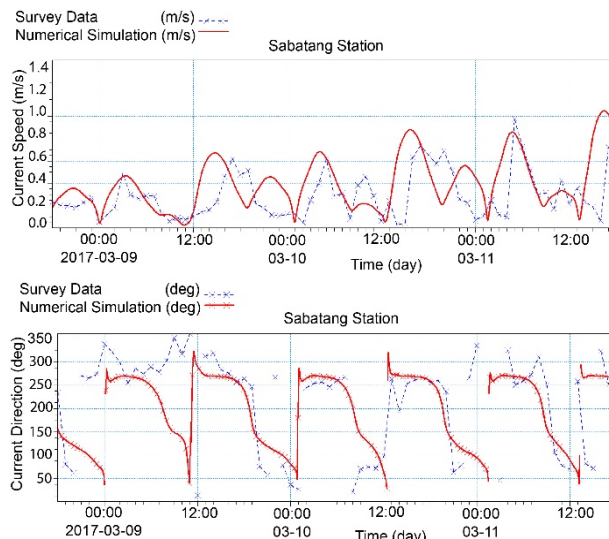


Fig. 5 Current velocity (RMS error: 0.18 cm/s within an acceptable criteria range of 0.2 m/s) and direction comparison between model simulation results and measurements at the SBT Station

The validation indicates that the model result is quantitatively within the criteria range.

3.2 Resource Assessment

Resource assessment is an important aspect of marine turbine deployment. It provides a scientific basis for the technology product selection suitable to the site-specific hydrodynamic conditions (water level, current and bathymetry). Based on the model simulation, the potential energy resources could be assessed by perceiving the energy distribution of the tidal current form. Figure 6 illustrates current speeds in PS location. The highest current speed is predominantly between SKI and BI. The statistic calculation indicates that the highest mean current speed at PS is up to 0.6 m/s (red colour) and reaches a maximum current speed reaches of 1.7 m/s. The mean current speed presents the highest mean resource around SBT, which is situated between BI and KI. The area between KI and PI also has a high mean current, although it is dispersed to a larger extent than that of SBT.

Figure 6 presents the pattern of the maximum current speed. The pattern of the highest current is still similar to that of the mean current speed, though a few peak spots appear in the southern part of KI up to 2.5 m/s. Based on these results, it can be determined that SBT has the most promising area to be developed. The maximum current speed is also situated not too far from the coastline. As the potential area is the closest to the coastline, SBT is one of the best places to be developed for marine tidal turbine in this region because with reduced distance from the coast, cost and risks of installation decrease. This condition can be used to consider the distance of turbine structures to the onshore.

In summary, the model simulation result indicates that the western part of SKI is a suitable location for the turbine deployment, where the mean current speed is around 0.5–0.6 m/s (Fig. 6A), and the maximum is more than 1.5 m/s (Fig. 6B). Because SKI is an inhabited island that is still developing its tourism and fishing industry, the spot area would be valuable to consider.

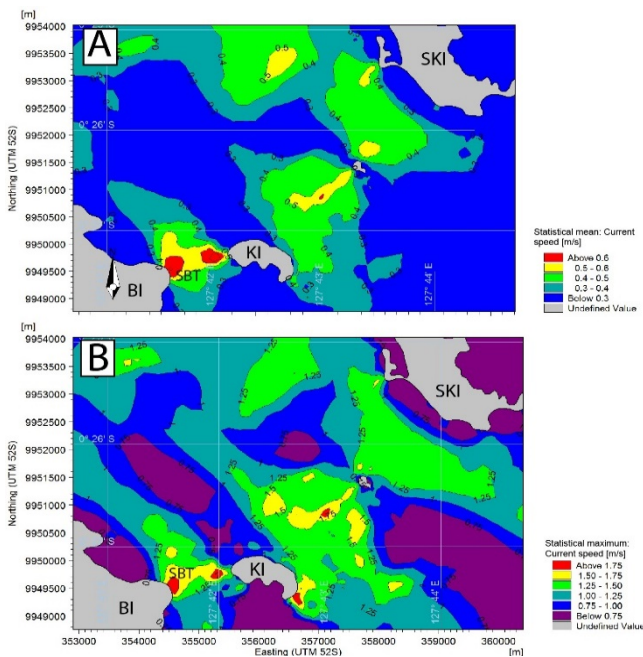


Fig. 6 Current Statistics (A: average current speed; B: maximum current speed)

Based on the current speed in Fig. 6A and Fig. 6B, the kinetic power density could be estimated. Resource estimation using the formula described by Bryden *et al.* (2007) yields the resource pattern illustrated in Fig. 7. In this figure, six observation points, P1 to P6, are determined by considering the closest to the coastline and the particularly water depth to illustrate the capacity of average kinetic power. Fig. 7A presents an average kinetic power density of the area between BI and KI, where the observation points were selected. This figure also illustrates a potential area to be developed (orange to red colours) within more than 0.12 kW/m². Four observation stations, P1, P2, P3 and P4, are selected to illustrate the potential of marine current turbines related to their cut-in speed (Table 1). The area with an average kinetic power density over 0.1 kW/m² covers approximately 234,810.00 m² (0.234 km²). This area is potentially suitable for the development of marine current energy to provide electricity to BI, where Labuha, the capital city of South Halmahera Regency, currently has a significant demand for energy.

Furthermore, Figure 7B presents the kinetic power density in the southern part of the PS, where the highest average kinetic power density is centred in the western part of SKI, albeit the amplitude is smaller than that in SBT. The highest kinetic power density is from 0.06 to 0.14 kW/m², and the total area has more than 0.1 kW/m² over approximately 198,750.00 m² (0.198 km²). Two observation points, P5 and P6, are also selected to illustrate marine current turbines' potential related to their cut-in speed, presented in Table 1.

Several marine turbine technologies that have been tested (e.g., De Groot, 2012); hence, European technologies would be considered to estimate potential energy yield (De Groot, 2012; Osalusi *et al.*, 2009). The devices recently reviewed by Rourke *et al.* (2010) classify two types of technology: tidal barrage and tidal current turbines. Generally, for a 1 MW capacity marine turbine, the cut-in speed is from 0.40 m/s to 1.00 m/s, whereas for a smaller-capacity turbine, around 300 kW, the cut-in speed is in the range of 0.20–0.40 m/s.

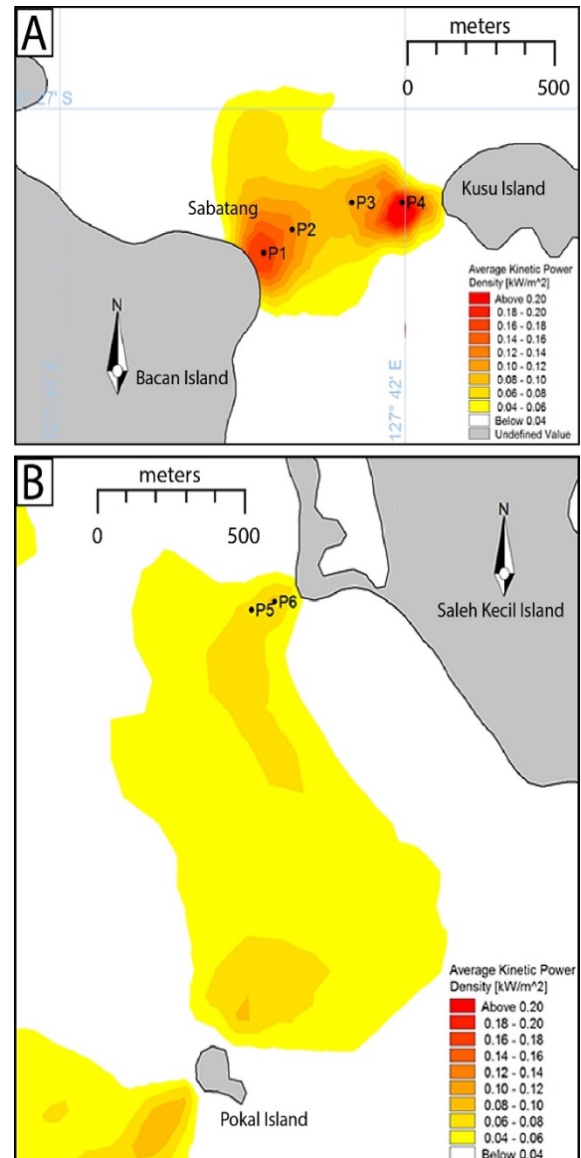


Fig. 7 Modelled spatial variation of average kinetic power density without depth limitation

Both capacities have different dimensions and technologies; consequently, each capacity has different water depth to be deployed. The high capacity requires deeper water depth than that of the low capacity. The low capacity is commonly installed in 10 m to 40 m of water depth, whereas the high capacity is installed between 40 and 100 m of water depth.

Figure 8 presents the location of high capacity of the average kinetic power, where the seabed contour overlays it from 40 to 100 m. As it can be seen in Fig. 8A, the area of average kinetic power density in SBT with more than 0.10 kW/m² is around 97,970 m², whereas in Fig. 8B, the area around SKI and PI reached 74,570 m² and 100,020 m², respectively.

Figure 9A illustrates the spatial variation of average kinetic power for the low-capacity condition in the SBT area. The area around BI with average kinetic power density of more than 0.10 kW/m² is 54,840 m², whereas in the KI part, it is 82,000 m². Close to PI and SKI areas, Fig. 9B illustrates the kinetic power density area spread to 10,320 kW/m² and 13,840 kW/m², respectively.

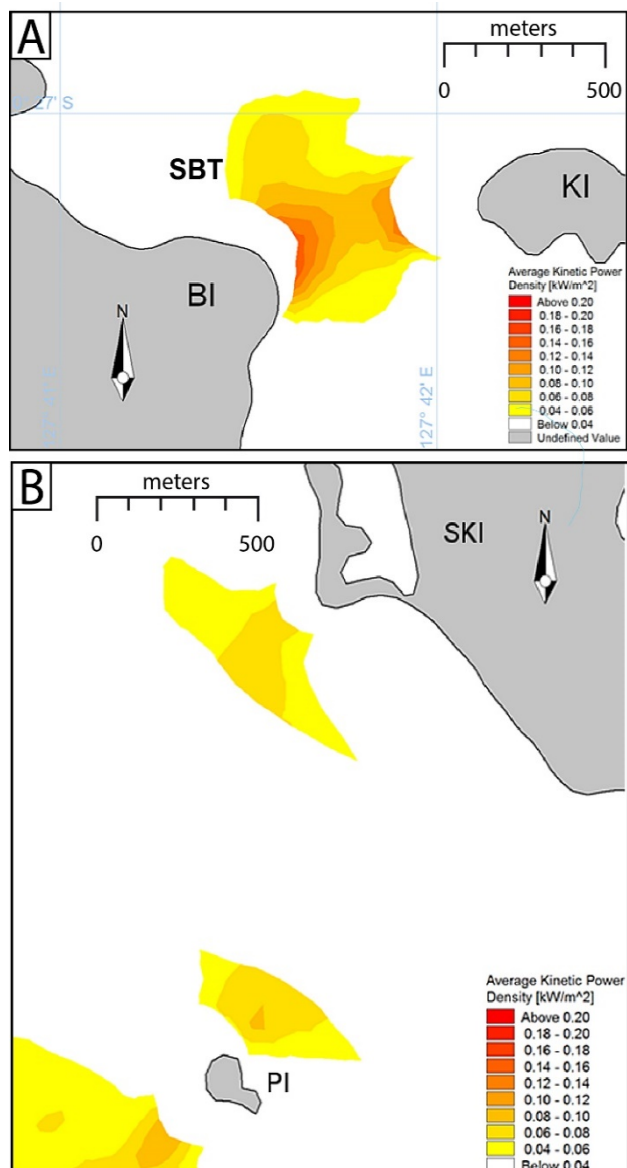


Fig. 8 Spatial variation for average kinetic power for the high-capacity condition (depth between 40 and 100 m)

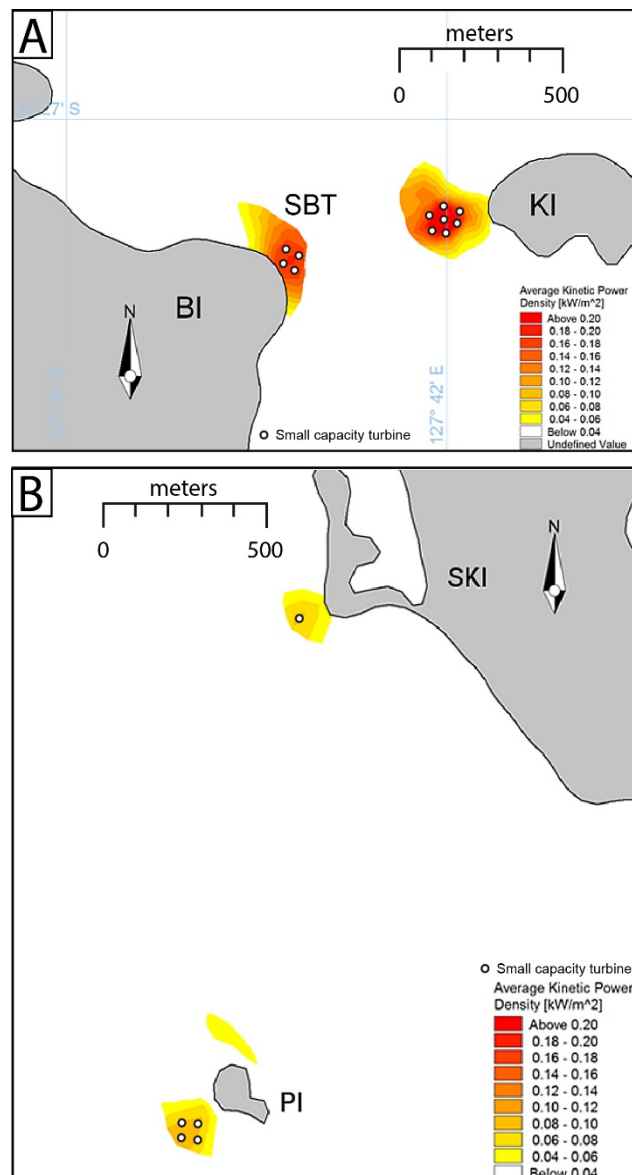


Fig. 9 Spatial variation of average kinetic power for the low-capacity condition (depth between 10 and 40 m)

Since the low capacity of the average kinetic power is much more promising because it has higher percentage of operational hours (Table 1), the design of small turbines is placed in P1, P4, P6 and the area near PI, Fig. 9B. These locations are considered by the water depth and the average kinetic potential that is realistic to adopt for small turbines (Fraenkel, 2006).

P1 is designed for four turbines to be arrays within 200 W/m² areas of less 40 m water depth. Furthermore, the turbine interval is adjusted within a 160 m length toward the offshore (Fig. 9A). P4 is near KI, which has a potential of 200 W/m² over more than 20,000 m² and at least seven small turbines can be placed within the interval of 70 m each and at 200 m toward to the offshore. P6 close to SKI has a smaller potential average kinematic power density than that in the area near PI, which is approximately 80 W/m², so one turbine is designed to be placed within less than 30 m water depth and 95 m from the coastline. Furthermore, the potential area near PI is planned to apply at least four small turbines within the interval 55 m and 100 W/m² kinematic power density.

Table 1 presents the availability percentage time duration as an energy resource based on the cut-in speed. Six stations are selected to represent the potential area, as illustrated in Fig. 7. The most operational points are P1 and P4, placed in SBT. In consideration the narrow width of this area, which is approximately 1 km, and the lack of renewable energy in BI, the area can be considered to be of high potential interest, and it is feasible to develop a marine energy project. Besides, P6 is a great location to be explored too as SKI is inhabited and is developing the tourism and fishery industry.

Table 1
 Percentage of running time based on cut-in speed

Station	Percentage of operational hours	
	Cut-in Speed: 0.2 m/s	Cut-in Speed: 0.4 m/s
P1	85.7	69.0
P2	82.9	64.7
P3	83.0	63.6
P4	91.3	74.7
P5	77.7	54.4
P6	83.8	58.3

In consideration of the average percentage of a small turbine, cut-in speed reaches 84%, whereas the larger turbine reaches 64%; hence, the practice of the small turbine is more promising. Areas of P1 and P4 that is closest to the BI and KI are of high priority and can be applied because the off-grid system will be much more economically and easily constructed than those in other locations.

3.3 Potential Impact

The energy resources harvested on the study sites potentially provide a platform of the development of the surrounding area. They will improve the local livelihood, such as basic needs, and offer opportunities for the local economic growth. However, it is also important to assess any environmental impact of the tidal turbine activities to the potential receptors in the area of interest. First, researchers have demonstrated that tidal turbines' energy extraction results in flow change from the turbine to a regional scale (Adcock *et al.*, 2015). In numerical modelling, the turbines' impact can be represented using the bottom friction method as demonstrated by Blunden and Bahaj (2015) or using the momentum sink approach performed by O'Brien *et al.* (2015). The bottom friction method is more practical. However, for the three-dimensional model, the latter option provides a more realistic simulation (Perez-Ortiz *et al.*, 2017).

The scale of water level and velocity changes depends on the installed turbine, where a larger array affects a more significant consequence. However, Draper *et al.* (2014) found that multiple arrays may increase one another's efficiency. Bed shear stress is also affected following the flow changes (Waldman *et al.*, 2017). Furthermore, Neill *et al.* (2009) demonstrated the possible impact of erosion and deposition around the turbines on the sediment dynamics at the site depending on the turbine scale.

Inger *et al.* (2009), Hastie *et al.* (2014), and Haslett *et al.* (2016) indicate that there is an interaction between marine biodiversity and the tidal turbine. Besides the environmental concern, it is also important to investigate the social impact. As a relatively new technology, public acceptance (Devine-Wright, 2011; Lim & Lam, 2014) and stakeholder engagement (Johnson *et al.*, 2013; Zydlewski *et al.*, 2014) are also required to successfully implement this technology.

4. Conclusion

This study used numerical modelling with inputs from *in situ* survey campaigns. The output of the numerical model simulation was then utilised for an energy resource assessment. Besides the magnitude of current speed derived from the model result, the energy estimation considers important parameters such as the depth and cut-in speed. The assessment results indicate that the tidal turbine is a potential source of energy in PS. The study also indicates that SBT holds the highest potential for energy resource in PS but is also famously known for its harsh condition; hence, the safety factor becomes an important parameter to consider. To move forward, a detailed study of the design aspects is especially required for tidal turbine technology prior the implementation of the design. Besides the battery saving, it is also an

important entity for maximising the energy because the operation hours still have a limitation.

It is important for further expansion to investigate the Indonesian Through-flow (ITF) components because the study area is within the ITF zone (Gordon, 2005). Meyer *et al.* (2014) demonstrated through-flow as a source of energy, suggesting that the ITF might be important to consider. Also, in future study, it is recommended to incorporate the speed reduction due to energy extraction by tidal turbines, which will yield a more realistic value for the generated power.

Author Contributions

Author Contributions: Conceptualisation, F.N. and E.H.S.; methodology, F.N. and D.M.; software, F.N, A.E. and M.M; model simulation and validation, A.E. and F.N.; formal analysis, F.N. and E.H.S.; investigation, E.H.S. and F.N.; resources, E.H.S, A.E and F.N.; data curation, D.M., E.H.S and M.M.; writing—original draft preparation, F.N. and E.H.S; writing—review and editing, F.N., E.H.S., D.M., AE and M.M.; visualisation, A.E., E.H.S., M.B.P and M.M; supervision, D.M.; project administration, E.H.S.; funding acquisition, F.N. and E.H.S. All authors have read and approved the published version of the manuscript.

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