



A Comparative Study of Advanced Oxidation Processes for Pentachlorophenol Degradation

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Abstract

Pentachlorophenol (PCP) is a priority pollutant that is highly resistant to conventional water treatment methods. Advanced Oxidation Processes (AOPs) offer an efficient approach by combining oxidants with activators to produce radicals. Hydrogen peroxide (H_2O_2) and peroxydisulfate ($S_2O_8^{2-}$) are oxidants with symmetrical peroxide bonds that effectively generate radicals through energy transfer. However, each produces distinct radicals, followed by different degradation mechanisms. A comprehensive comparison is crucial for adopting effective AOP technologies. This study evaluates the kinetic performance and cost-effectiveness of AOPs using H_2O_2 and $S_2O_8^{2-}$, activated by ultrasound (US), UV light (UVC and VUV), and their combinations. H_2O_2 demonstrated superior performance, particularly under UV light, due to its pH stability and higher reactivity with PCP. The combination of US and VUV irradiation resulted in the highest degradation rates, with the addition of H_2O_2 yielding the best overall performance ($k = 0.75 \text{ min}^{-1}$). Increasing the temperature enhanced PCP degradation across all systems, with the US-VUV- H_2O_2 system achieving the highest rate at 35°C ($k = 0.91 \text{ min}^{-1}$). The VUV- H_2O_2 system recorded the lowest activation energy ($E_a = 4.77 \text{ kJ mol}^{-1}$), indicating greater efficiency. H_2O_2 -based systems, particularly VUV- H_2O_2 and UVC- H_2O_2 , emerged as the most efficient and cost-effective options, with the lowest energy consumption (4.65–4.80 kWh m^{-3}) and costs (Rp8,825–Rp9,064/ m^{-3}). These results highlight H_2O_2 in UV configurations as the optimal choice for PCP degradation, offering effective treatment with reduced energy and chemical requirements.

1. Introduction

Pentachlorophenol (PCP), a highly chlorinated hydrocarbon, has been extensively used as a wood preservative and biocide [1]. Its chemical stability has contributed to extensive contamination of both terrestrial and aquatic ecosystems, enabling its accumulation and transmission through the food chain [2]. Furthermore, PCP's acute and chronic toxicity, along with its carcinogenic properties, have led to its classification as a priority pollutant by the US EPA, with a maximum contaminant level of 0.001 mg/L for drinking water [3]. In Indonesia, the permissible PCP concentration in drinking water is set at 0.009 mg/L [4]. Given these factors, the removal of PCP is crucial in water reclamation processes. Both biological and chemical methods have been explored for PCP remediation.

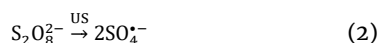
However, PCP is considered one of the most toxic and treatment-resistant compounds when using conventional activated sludge processes [3]. Advanced oxidation processes (AOPs) have demonstrated significant effectiveness in degrading chlorophenols and chlorobenzenes, making them a promising approach for PCP remediation [5].

AOPs involve the combination of oxidants, such as hydrogen peroxide H_2O_2 or persulfate salts, with activators to generate highly reactive free radicals. Persulfate salts are commonly found in the form of peroxymonosulfate (HSO_5^-) and peroxydisulfate ($S_2O_8^{2-}$). These radicals effectively degrade pollutants by breaking them down into less harmful substances through a process known as mineralization [6]. The generation of free radicals occurs in situ via energy or electron transfer

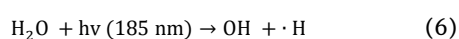
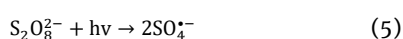
reactions. Energy-activated AOPs are highly effective at rapidly breaking down persistent pollutants without the use of harsh chemicals, thereby minimizing the risk of secondary pollution [7, 8]. This efficiency is further enhanced when symmetrical peroxide oxidants, such as H_2O_2 and $\text{S}_2\text{O}_8^{2-}$, are used. These oxidants undergo homolytic cleavage of the peroxide ($-\text{O}-\text{O}-$) bond, resulting in the formation of two identical radicals, hydroxyl radicals ($\cdot\text{OH}$) or sulfate radicals ($\text{SO}_4^{\cdot-}$), which serve as the primary oxidants [9].

Both $\cdot\text{OH}$ and $\text{SO}_4^{\cdot-}$ radicals are highly reactive and capable of oxidizing a wide range of organic compounds; however, the mechanisms by which they degrade pollutants can differ significantly. $\text{SO}_4^{\cdot-}$ primarily reacts through electron transfer reactions, whereas $\cdot\text{OH}$ can also engage in hydrogen-atom abstraction in addition to electron transfer [10]. These distinct reaction pathways lead to varying degradation efficiencies and outcomes. Consequently, understanding and evaluating the differences in performance between the two symmetrical oxidants, H_2O_2 and $\text{S}_2\text{O}_8^{2-}$, is essential. These oxidants generate unique radicals and follow different mechanisms, which can profoundly impact their effectiveness in treating specific pollutants.

Energy inputs for AOPs encompass ultrasound, light, and heat. US irradiation, recognized for its environmental compatibility and effectiveness, operates by inducing cavitation in liquids at frequencies ranging from 20 to 1,000 kHz. This process involves the formation, growth, and collapse of bubbles, releasing extreme localized conditions—temperatures up to 5,000 K and pressures reaching 1,000 atm—which activate oxidants to produce free radicals [11], as shown in Equations (1) and (2). Additionally, ultrasound can break water molecules to generate hydroxyl radicals, as described in Equation (3).



Similarly, light energy plays a critical role in photochemical AOPs, where UV light in the range of ~200–280 nm effectively promotes the generation of $\cdot\text{OH}$ or $\text{SO}_4^{\cdot-}$ radicals. UV-based processes are considered clean, simple, and often more efficient than purely chemical AOPs [7]. UVC light is commonly used, though to further enhance radical production, vacuum-UV (VUV) light is employed, which emits wavelengths of 185 nm and 254 nm simultaneously [12]. The chemical reactions representing radical formation by UV-based AOPs are presented in Equations (4) and (5). Moreover, VUV-185 nm light is highly absorbed by water (with an absorption coefficient of 1.8 cm^{-1}), making it particularly effective for activating water molecules to generate radicals efficiently [13], as illustrated in Equation (6).



Considering the predominant yet distinct mechanisms involved in AOPs using H_2O_2 and $\text{S}_2\text{O}_8^{2-}$ activated by US and ultraviolet light (UVC and VUV), or their combinations, understanding the effectiveness of each approach is essential for evaluating performance and applicability. Previous studies have mostly examined these processes individually. For instance, H_2O_2 and $\text{S}_2\text{O}_8^{2-}$ activated by US were compared for the removal of phenol from aqueous solutions, with results indicating that the combination of US/ $\text{S}_2\text{O}_8^{2-}$ achieved the highest efficiency, exceeding 90% [14]. UV/ H_2O_2 and UV/ $\text{S}_2\text{O}_8^{2-}$ processes have also been evaluated for degrading acetamiprid, where the UV/ $\text{S}_2\text{O}_8^{2-}$ process showed the best performance, with a rate constant of 0.11 min^{-1} [15].

In another study, the individual and combined effects of UV and US in activating $\text{S}_2\text{O}_8^{2-}$ were investigated for the degradation of tetracycline in aqueous solution. The highest removal efficiency—approximately 96.29%—was achieved using the combined UV/US/ $\text{S}_2\text{O}_8^{2-}$ process, outperforming the individual treatments [16]. Since energy-activated AOPs are seen as effective and environmentally friendly for contaminant removal, assessing their energy consumption is crucial for evaluating economic feasibility. Although energy-per-order comparisons of various AOPs have been reported [17], persulfate-based systems were not included. Furthermore, most prior studies evaluated H_2O_2 and $\text{S}_2\text{O}_8^{2-}$ activation separately, under different conditions, targeting different pollutants, and using varying evaluation parameters—making fair comparisons difficult.

Although several review papers have discussed sonolytic and photolytic AOPs [18, 19, 20, 21], direct experimental comparisons conducted under uniform conditions remain scarce. Therefore, a systematic investigation into both the individual and combined effects of these AOPs under standardized experimental settings is essential to accurately evaluate their degradation kinetics and economic feasibility. To date, no single study has comprehensively assessed these aspects within a unified experimental framework. This study aims to address this gap by providing a thorough comparison of various energy-activated AOPs for the degradation of PCP, contributing valuable insights for the effective implementation of AOP technologies in the treatment of PCP-contaminated wastewater.

2. Experimental

2.1. Chemicals and Reagents

All chemicals used in the experiments were of analytical reagent grade. Pentachlorophenol ($\text{C}_6\text{Cl}_5\text{OH}$, 97%) and sodium persulfate ($\text{Na}_2\text{S}_2\text{O}_8^{2-}$, 99%) were purchased from Sigma-Aldrich Inc., USA. Hydrogen peroxide (H_2O_2 , 35%) was obtained from Daejung Chemicals & Metals, Korea. Temperature regulation was achieved using a cooling system. Water used for reagent preparation was purified using a Millipore reverse osmosis system with a resistivity of $18.2 \text{ M}\Omega\cdot\text{cm}$. Acetic acid (CH_3COOH , 100%, HPLC grade) was purchased from J.T. Baker Chemical Co., and acetonitrile (99.9%, HPLC grade) was purchased from Duksan Pure Chemical Co.

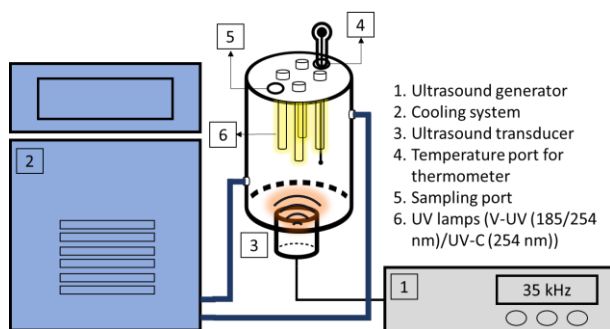


Figure 1. Reactor setup for photolytic and sonolytic experiments

2.2. Experimental Setup and Analysis Method

The experimental setup for the photolytic and sonolytic degradation of PCP is illustrated in Figure 1. The degradation experiments were conducted in a capped cylindrical glass batch reactor (ϕ 100 × H 200 mm, total volume: 1.50 L, experimental volume: 1 L). A single piezoelectric transducer with an area of approximately 1590.4 mm² (PZT, Tamura, Japan) was installed beneath the reactor to irradiate ultrasound from the bottom. The transducer was connected to an ultrasonic generator (Mirae Ultrasonic MEGA-100, Korea), allowing control of the power and frequency, set at 35 kHz and 70 W, respectively. For photolytic experiments, the reactor was equipped with either four UVC lamps (254 nm, 10 W each) or four VUV lamps (185/254 nm, 10 W each), each measuring 150 mm in length. The lamps were partially submerged, with approximately 77.3 mm of their length in contact with the water. The temperature of the reactor was maintained using a water jacket surrounding the reactor to ensure stable operating conditions.

At specific time intervals, 1 mL of the solution was sampled, filtered through a 0.22 μ m Millipore membrane, and mixed with 1 mL of methanol to completely terminate the oxidation process. The experiments were conducted as single runs; therefore, the results primarily serve as preliminary comparative data to highlight trends. The PCP concentration was analyzed using a high-performance liquid chromatography (HPLC) system (Agilent 1260 Infinity) equipped with a Poroshell 120 EC-C18 column (4.6 × 150 mm, 5 μ m) and a diode array detector set at 300.5 nm. The mobile phase consisted of 70% acetonitrile and 30% aqueous acetic acid (5%), delivered at a flow rate of 1 mL/min [22].

2.3. Kinetic Analysis

The residual concentration of PCP in the solution was used to determine the kinetic constants. The kinetic constants were derived using the pseudo-first-order kinetic model, considering that it is commonly applied in AOPs research [23, 24, 25]. In addition, this model was chosen due to the condition in which the oxidant is used in excess compared to the target contaminant. In this experiment, the initial concentration of PCP and the concentrations of oxidants (either H₂O₂ or S₂O₈²⁻) corresponded to a 1:10 ratio. Under such conditions, the concentration of the oxidant is assumed to remain relatively constant throughout the reaction, and the reaction rate depends primarily on the concentration of

PCP. The equation for the pseudo-first-order kinetic model is represented in Equation (7).

$$\frac{dC}{dt} = -k_1 C \quad (7)$$

Where, *C* represents the concentration of PCP, *t* denotes time, and *k* is the kinetic constant. The activation energy parameters for PCP decomposition were determined using the Arrhenius equation (Equation (8)).

$$\ln k = \ln A - \left(\frac{E_a}{RT}\right) \quad (8)$$

Where, *A* is the Arrhenius constant, *R* is the universal gas constant (8.3144598 J mol⁻¹K⁻¹), *T* refers to the absolute temperature (K), *k* represents the reaction rate constant (min⁻¹), *E_a* denotes the activation energy (kJ mol⁻¹). This equation was applied in the *lnk* vs. $\frac{1}{T}$ format, where the slope gives the value of $\frac{-E_a}{R}$ from where *E_a* can be calculated.

3. Results and Discussion

3.1. Effect of Different Combinations of Oxidant and Energy Input

Figure 2 illustrates the kinetic rate constant (*k*) of PCP degradation for various combinations of oxidants (H₂O₂ and S₂O₈²⁻) activated by different energy inputs, including US, VUV, UVC, US-VUV, and US-UVC. The complete kinetic degradation profiles of PCP over time are presented in Figure S1.

When comparing H₂O₂ and S₂O₈²⁻ as oxidants, H₂O₂ consistently outperforms S₂O₈²⁻ in most energy activation methods, particularly those involving light-based activation (VUV, UVC, US-VUV, and US-UVC), as evidenced by the higher *k* values. These results align with previous studies that demonstrated higher *k* for clonidine, benzoic acid, and nitrobenzene under UV/H₂O₂ systems compared to UV/S₂O₈²⁻ systems [26, 27]. Similarly, UV/H₂O₂ achieved better removal efficiency than HSO₅⁻-based systems for 23 tested micropollutants [28].

The first explanation is likely due to the fact that this system operates at nearly neutral pH. H₂O₂ is more stable and effective across a wider pH range (typically pH 3–9), making it well-suited for neutral conditions. In contrast, S₂O₈²⁻ performance is more pH-dependent and typically requires acidic conditions (pH < 3) for optimal activation [26]. This highlights the practical advantage of H₂O₂ for real-world applications under neutral pH conditions, where S₂O₈²⁻ efficacy may be limited.

Furthermore, PCP exhibits higher reactivity with ·OH than with SO₄⁻. This difference can be attributed to PCP's molecular structure: the five chlorine atoms attached to the benzene ring reduce the oxidation state of the carbon atoms, making them more susceptible to attack by ·OH. ·OH are known to preferentially target carbon atoms with lower oxidation states in the early stages of the degradation process, which explains the superior degradation kinetics achieved with H₂O₂ as the oxidant [29].

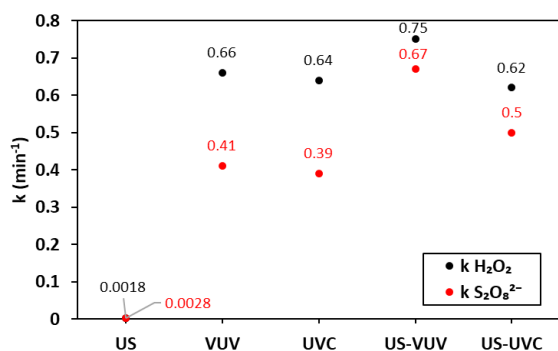


Figure 2. Kinetic constant of PCP degradation using different combinations of oxidant and energy input ([PCP]₀ = 10 mg/L; [H₂O₂]₀/[S₂O₈²⁻]₀ = 0.4 mM; US frequency = 35 kHz; US power = 70W; UV power = 10 W(each); T = 25°C; and initial pH = 6 ± 0.2)

However, under US activation alone, S₂O₈²⁻ achieves a higher k value of $k = 0.0028 \text{ min}^{-1}$ compared to H₂O₂ ($k = 0.0018 \text{ min}^{-1}$). This indicates that the cavitation effects generated by US are more effective at S₂O₈²⁻ to produce SO₄^{•-} than at activating H₂O₂ to generate •OH [23, 30]. UV light activates S₂O₈²⁻ through photolysis, which depends on the direct absorption of UV photons by molecules. The molar absorption coefficient (ϵ) of S₂O₈²⁻ at a UV wavelength of 254 nm is $21.1 \text{ M}^{-1}\text{cm}^{-1}$, slightly higher than that of H₂O₂ ($\epsilon = 18.6 \text{ M}^{-1}\text{cm}^{-1}$) [31, 32].

In terms of energy inputs to activate oxidants, the US alone results in the lowest k for both oxidants. In contrast, both VUV and UVC light significantly enhance k . For H₂O₂, the k reaches 0.66 min^{-1} with VUV and 0.64 min^{-1} with UVC, while for S₂O₈²⁻, the k values improve to 0.41 min^{-1} (VUV) and 0.39 min^{-1} (UVC). UV activation provides consistent, high-energy photons that efficiently cleave peroxide bonds through photolysis, ensuring rapid and uniform radical generation. This is attributed to both oxidants' strong absorption of UVC light at 254 nm and even higher absorption at VUV wavelengths (185 nm), which deliver more energetic photons for effective bond cleavage. For instance, H₂O₂ has an absorption coefficient of approximately $240 \text{ M}^{-1}\text{cm}^{-1}$ at 185 nm, significantly higher than its absorption at 254 nm ($18.6 \text{ M}^{-1}\text{cm}^{-1}$). Similarly, S₂O₈²⁻ demonstrates a much stronger absorption at 185 nm, with an absorption coefficient of approximately $350 \text{ M}^{-1}\text{cm}^{-1}$, compared to $21.1 \text{ M}^{-1}\text{cm}^{-1}$ at 254 nm [33, 34].

Combining US with VUV energy inputs achieves the highest k for PCP degradation. For H₂O₂, the k reaches 0.75 min^{-1} , while for S₂O₈²⁻, k increases to 0.67 min^{-1} . This synergistic effect arises from the physical effect of cavitation, which provides the intense mixing to utilize the UV light irradiation effectively [35, 36, 37, 38]. Among all tested configurations, the combination of H₂O₂ with US-VUV delivers the highest k , showcasing the powerful synergy between ultrasound and VUV light. Although S₂O₈²⁻ also performs effectively, it generally shows slightly lower k , likely due to the slower reaction mechanisms associated with SO₄^{•-} compared to •OH. This

highlights the superior performance of H₂O₂ in energy-activated AOP systems, particularly under combined US-VUV conditions.

3.2. Effect of Initial Temperature

Temperature is a critical factor in redox systems, as it directly influences the activation energy required to initiate the reaction. To evaluate the effect of temperature on PCP degradation, experiments were conducted at 15, 25, and 35°C. The choice of these temperatures represents different environmental and operational scenarios: 25°C reflects average ambient temperatures in temperate regions and standard laboratory conditions, 15°C simulates colder environments or industrial settings with cooling systems, and 35°C represents warmer climates or tropical regions. This range allows for a comprehensive understanding of how temperature impacts the efficiency of the degradation process.

The effect of temperature on PCP degradation shows a clear trend of increased degradation rates with rising temperatures for both H₂O₂ and S₂O₈²⁻ across various energy activation methods, as shown in Figure 3(a) for H₂O₂ and 3(b) for S₂O₈²⁻. The highest k achieved in the US-VUV-H₂O₂ system, where k reaches 0.91 min^{-1} at 35°C. The observed enhancement in degradation rates with increasing temperature can be attributed to its role in lowering activation energy. Elevated temperatures facilitate faster cleavage of peroxide bonds and improve radical formation efficiency in both H₂O₂ and S₂O₈²⁻ systems [39]. This effect is particularly pronounced in systems employing VUV or US-VUV, where the combination of photolysis, cavitation, and thermal effects enhances radical generation and reaction kinetics [20].

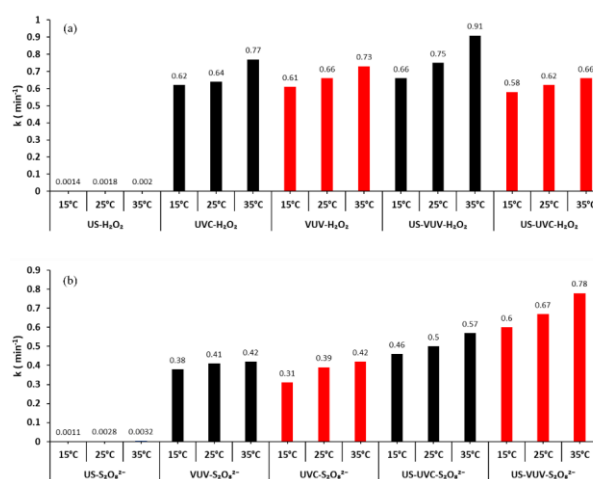


Figure 3. Kinetic constant of PCP degradation using various energy input at various temperature to activate (a) H₂O₂, and (b) S₂O₈²⁻ ([PCP]₀ = 10 mg/L; [H₂O₂]₀/[S₂O₈²⁻]₀ = 0.4 mM; US frequency = 35 kHz; US power = 70W; UV power = 10 W (each); and initial pH = 6 ± 0.2)

Table 1. Economic comparison of PCP degradation in distilled water by various AOPs systems

System	E_{EO} (kWh m ⁻³)	Oxidant conc. (mM)	Cost		Total cost (/m ⁻³)
			Electricity (kWh ⁻¹)	Chemical (kg ⁻¹)	
US-S ₂ O ₈ ²⁻	1920.00	0.004	Rp3,157,478	Rp1,090,000	Rp4,247,478
VUV-S ₂ O ₈ ²⁻	7.49	0.004	Rp12,322	Rp1,090,000	Rp1,102,322
UVC-S ₂ O ₈ ²⁻	7.88	0.004	Rp12,954	Rp1,090,000	Rp1,102,954
US-VUV-S ₂ O ₈ ²⁻	12.61	0.004	Rp20,736	Rp1,090,000	Rp1,110,736
US-UVC-S ₂ O ₈ ²⁻	16.90	0.004	Rp27,786	Rp1,090,000	Rp1,117,786
US-H ₂ O ₂	2986.67	0.004	Rp4,911,633	Rp1,171	Rp4,912,804
VUV-H ₂ O ₂	4.65	0.004	Rp7,654	Rp1,171	Rp8,825
UVC-H ₂ O ₂	4.80	0.004	Rp7,894	Rp1,171	Rp9,064
US-VUV-H ₂ O ₂	11.26	0.004	Rp18,524	Rp1,171	Rp19,695
US-UVC-H ₂ O ₂	13.63	0.004	Rp22,408	Rp1,171	Rp23,579

Condition: [PCP]₀ = 10 mg/L; [H₂O₂]₀/[S₂O₈²⁻]₀ = 0.4 mM; US frequency = 35 kHz; US power = 70W; UV power = 10 W(each); T = 25°C; and initial pH = 5.8 ± 0.2.

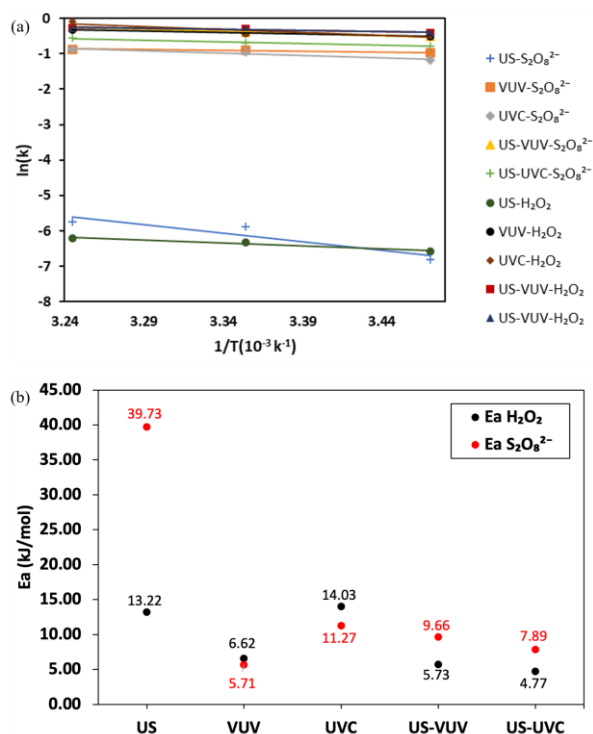


Figure 4. Arrhenius plot of the pseudo first order rate constants, and (b) activation energy of PCP degradation using different combinations of oxidant and energy input ([PCP]₀ = 10 mg/L; [H₂O₂]₀/[S₂O₈²⁻]₀ = 0.4 mM; US frequency = 35 kHz; US power = 70W; UV power = 10 W(each); T = 25°C; and initial pH = 6 ± 0.2)

The Arrhenius equation was applied to calculate E_a value. Activation energy refers to the minimum energy required to initiate a chemical reaction. The Arrhenius plots for all the systems are given in Figure 4(a), which accordingly shows that k increases with an increase in temperature. The calculated E_a for PCP decomposition using all combinations of oxidant and energy inputs is shown in Figure 4(b). The highest E_a is observed in the US system with S₂O₈²⁻ (E_a = 39.73 kJ mol⁻¹), indicating the limited efficiency of the US alone in activating S₂O₈²⁻ for SO₄^{•-} generation. This value is in the order of magnitude of previously reported tetracycline degradation using the same system, with a value of E_a of 32.01 kJ mol⁻¹ [40].

In contrast, the lowest E_a is recorded in the US-UVC system with H₂O₂ (E_a = 4.77 kJ mol⁻¹), which is eight times lower than US activated alone. Furthermore, compared to other reported PCP degradation methods, such as heat-activated persulfate (E_a = 105.60 kJ mol⁻¹) [41] and H₂O₂ activated by magnetite (E_a = 47.00 kJ mol⁻¹) [42], the US-UVC system demonstrates a significantly lower energy requirement. This highlights the strong synergistic effect of combining US cavitation with UV light, which effectively reduces the energy barrier for •OH production.

3.3. Energy and Cost Comparison

An economic evaluation of the AOP systems in this study was conducted using the electrical energy per order (E_{EO}) metric. E_{EO} is a quantitative parameter used to assess the energy consumption of AOPs, aiding both technical development and practical applications. It represents the amount of electrical energy, measured in kilowatt-hours (kWh), required to degrade a contaminant concentration (C) by one order of magnitude in a unit volume, such as 1 m³ (1000 L), of contaminated water. E_{EO} is particularly suitable for scenarios where the contaminant concentration is low, and the reaction follows first-order kinetics with respect to C. This makes it highly relevant to this study, as PCP is classified as a micropollutant [43]. In this study, E_{EO} (kWh m⁻³) of an idealized batch reactor was calculated using Equation (9).

$$E_{EO} = \frac{P_{38.4}}{V \cdot k} \quad (9)$$

Where, P represents the input power (kW) of the US, UVC, and/or VUV utilized in each system, V denotes the volume of treated water (L), and k corresponds to the first-order rate constant (min⁻¹).

Furthermore, the cost analysis in Indonesian Rupiah was conducted based on the calculated E_{EO} values and is summarized in Table 1. The electricity price per kWh was determined using the rates set by the Indonesian National Electricity Company (PLN) as of January 2025, while the chemical costs were derived from the per-kilogram pricing of Sigma Aldrich products. A detailed summary of the economic comparison to treat 1 m³ of PCP-contaminated water is presented in Table 1.

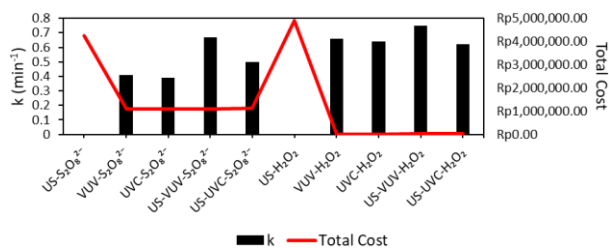


Figure 5. Plot of reaction rate constants for PCP degradation using various AOP methods versus treatment costs for each method

The most efficient and cost-effective systems are VUV-H₂O₂ (4.65 kWh/m³, Rp8,825/m³) and UVC-H₂O₂ (4.80 kWh/m³, Rp9,064/m³), which have the lowest E_{EO} values and total costs. In contrast, persulfate systems like US-S₂O₈²⁻ show the highest E_{EO} (1920 kWh m⁻³) and total cost (Rp4,247,478/m³), making it the least economical option. While UV-based S₂O₈²⁻ systems (VUV-S₂O₈²⁻ and UVC-S₂O₈²⁻) are more efficient, they still have higher total costs compared to H₂O₂ systems. Overall, H₂O₂, particularly in UV configurations, proves to be the most energy-efficient and cost-effective choice for treating PCP-contaminated water, as illustrated in Figure 5. It is also evident that H₂O₂ use is more economical than UV/S₂O₈²⁻ systems due to the high cost of persulfate.

Previously reported results have shown that the E_{EO} amount for US is 31.72 times more than that combination with UV for H₂O₂-based AOPs [44], which aligns with the findings of this study. Furthermore, E_{EO} values for various pharmaceuticals and personal care products treated by UV/H₂O₂ have been reported to range from 0.017 to 2.26 kWh/m³ [45], while for UV/S₂O₈²⁻, the values for degradation of heliotrine and its N-oxide were 0.28 and 0.43 kWh/m³, respectively [46]. The results of this study offer a more comprehensive comparison of the energy requirements for each method. This leads to the recommendation of UV combined with H₂O₂ as the most environmentally and economically favorable option—minimizing both electricity and chemical consumption while ensuring rapid pollutant degradation.

4. Conclusion

This study compares various AOPs, including combinations of H₂O₂ and S₂O₈²⁻ activated by US and UV light (UVC and VUV), or their combinations, to degrade PCP in distilled water. The comparison focuses on kinetic performance and cost-effectiveness. H₂O₂ generally outperforms S₂O₈²⁻, especially under UV activation, due to its better pH stability and better reactivity with ·OH. While S₂O₈²⁻ shows higher k with US alone, its performance is limited by pH dependence and slower reaction speeds. The combination of US and VUV activation produces the highest k for both oxidants, with H₂O₂ showing the best overall results ($k = 0.75 \text{ min}^{-1}$). Higher temperatures improve PCP degradation for all the systems, with the highest rate ($k = 0.91 \text{ min}^{-1}$) observed in the US-VUV-H₂O₂ system at 35°C. The lowest activation energy (E_a 4.77 kJ·mol⁻¹) was found in the US-UVC-H₂O₂ system, indicating higher efficiency. H₂O₂-based systems, particularly VUV-H₂O₂ and UVC-H₂O₂, demonstrated the highest efficiency and cost-effectiveness, with the lowest

E_{EO} values (4.65–4.80 kWh m⁻³) and treatment costs (Rp8,825–Rp9,064/m³). This study highlights H₂O₂, especially in UV configurations, as the best choice for PCP degradation, offering reduced energy use, lower chemical consumption, and effective treatment. The study provides valuable insights into the efficiency of different AOPs for PCP degradation, but it has some limitations. Specifically, it does not explore radical production or the formation of intermediate products, which are important for understanding the degradation mechanism. Additionally, the type of interaction between combined AOPs—whether synergistic, additive, or antagonistic—was not quantitatively assessed, which could offer a deeper understanding of their combined effects. Future research should focus on these aspects, including synergy analysis, to optimize AOPs and improve their application to other contaminants.

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